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# A MATLAB-based graphical user interface program for computing functionals of the geopotential up to an arbitrary degree and order<sup>☆</sup>

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## Abstract

We present a novel graphical user interface program GrafLab (GRAVity Field LABoratory) for spherical harmonic synthesis (SHS) created in MATLAB<sup>®</sup>. This program allows to comfortably compute 18 various functionals of the geopotential up to an arbitrary degree and order of spherical harmonic expansion. For the most difficult part of the SHS, namely the evaluation of the fully normalized associated Legendre functions (fnALFs), we used three different approaches according to required maximum degree: (i) the standard forward column method (up to maximum degree 1 800, in some cases up to degree 2 190); (ii) the modified forward column method combined with Horner's scheme (up to maximum degree 2 700); (iii) the extended-range arithmetic (up to an arbitrary maximum degree). For the maximum degree 2 190, the SHS with fnALFs evaluated using the extended-range arith-

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<sup>☆</sup>Code available from [http://www.svf.stuba.sk/en/departments/departments-of-theoretical-geodesy/science-and-research/downloads.html?page\\_id=4996](http://www.svf.stuba.sk/en/departments/departments-of-theoretical-geodesy/science-and-research/downloads.html?page_id=4996)

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metic approach takes only approximately 2-3 times longer than its standard arithmetic counterpart, i.e. the standard forward column method. In the GrafLab, the functionals of the geopotential can be evaluated on a regular grid or point-wise, while the input coordinates can either be read from a data file or entered manually. For the computation on a regular grid we decided to apply the lumped coefficients approach due to significant time-efficiency of this method. Furthermore, if a full variance-covariance matrix of spherical harmonic coefficients is available, it is possible to compute the commission errors of the functionals. When computing on a regular grid, the output functionals or their commission errors may be depicted on a map using automatically selected cartographic projection.

*Keywords:* Geopotential model, Gravity field functional, Spherical harmonic synthesis, Lumped coefficients, Commission error, Extended-range arithmetic

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## 1 Introduction

In geodesy, the spherical harmonic expansion (SHE) is widely used for the determination of the Earth's external gravity field. The spherical harmonics provide an efficient mathematical tool for computing an arbitrary functional of the geopotential referred to a point lying on the Earth's surface or aloft; this process is known as the spherical harmonic synthesis (SHS). By definition, a functional is a special case of an operator, which associates to a function a real number (Moritz, 1980; Rektorys, 1999). The most common functionals of the geopotential are geoid undulation, height anomaly, gravity anomaly, gravity disturbance and deflections of the vertical. Nowadays,

11 the computation of these and many other functionals up to degree 2 190 is  
12 possible using the global geopotential model of the Earth (GGM) EGM2008  
13 (Pavlis et al., 2012) and it can be expected that in the future the maxi-  
14 mum degree of GGMs will continue to increase. However, hand in hand with  
15 the increasing degree of SHE, some numerical problems associated with the  
16 computation of spherical harmonics occur.

17 The principal problem in the computation of spherical harmonics of high  
18 degrees and orders is the numerical evaluation of associated Legendre func-  
19 tions of the first kind (ALFs)  $P_{nm}(\cos \theta)$  (Hoffmann-Wellenhof and Moritz,  
20 2005), which depend on the spherical co-latitude  $\theta$ . Hence, ALFs are usually  
21 used in the fully normalized form (ibid.), which is algebraic method avoiding  
22 the numerical problems, so one obtains the fully normalized associated Leg-  
23 endre functions (fnALFs)  $\overline{P}_{nm}(\cos \theta)$ . However, for very high degrees and  
24 orders (e.g. 2 700), fnALFs still range over thousands of orders of magni-  
25 tude and under-flow or over-flow problems occur (Holmes and Featherstone,  
26 2002b). Some special care has to be put on the numerical evaluation of  
27 fnALFs. Thus, the standard recursive algorithms for computing values of  
28 fnALFs (cf. Colombo, 1981; Holmes and Featherstone, 2002b) have to be  
29 modified.

30 Holmes and Featherstone (2002b) presented an effective approach, which  
31 allows to compute fnALFs up to degree and order 2 700 for all co-latitudes  
32 without any under-flow or over-flow problems. This method is based on two  
33 factors: (i) eliminating the problematic term  $\sin^m(\theta)$  from the recursions, so  
34 one obtains the scaled values of fnALFs  $\overline{P}_{nm}(\cos \theta)/\sin^m(\theta)$ ; (ii) introducing  
35 a global scale factor of  $10^{-280}$ . This two factors may be introduced into the

36 standard recursions obtaining the modified recursions, see e.g. Holmes and  
37 Featherstone (2002b). Once the scaled values of the fnALFs are obtained,  
38 the problematic term  $\sin^m(\theta)$  is gradually re-introduced employing Horner's  
39 scheme and finally, after multiplication by the reciprocal value of the global  
40 scale factor, the non-scaled values of fnALFs are obtained.

41 These modified recursions are numerically stable up to the degree and  
42 order 2 700. For even higher degrees and orders, under-flow or over-flow  
43 problems occur again. Thus, this approach is also limited. Fukushima (2011)  
44 has introduced another approach, which enables to compute fnALFs up to  
45 extremely high degree such as  $2^{32} = 4\,294\,967\,296$ , by modifying the idea  
46 of extended-range arithmetic (Smith et al., 1981). In extended-range arith-  
47 metic, a non-zero arbitrary real number  $X$  is expressed as  $X = x B^{i_X}$ , where  
48  $B$  is the radix (a large power of 2),  $x$  is the significand and  $i_X$  is the exponent.  
49 Another words, a separate storage location to the exponent of each floating-  
50 point number is allocated (Wittwer et al., 2008). In the double-precision  
51 Fukushima (2011) used the radix value  $B = 2^{960}$ . Hence, much bigger and  
52 smaller numbers can be represented in the IEEE (Institute of Electrical and  
53 Electronic Engineers') double-precision, so fnALFs of an arbitrary degree and  
54 order can be evaluated using the standard recursions without an under-flow  
55 problem. For more details about the extended-range arithmetic, the reader  
56 is advised to Fukushima (2011) or Smith et al. (1981).

57 Several computer programs for evaluating various functionals of the geopo-  
58 tential have been developed so far, e.g. Holmes and Pavlis (2008); Janák and  
59 Šprlák (2006); Sanso and Sona (2001); Smith (1998); Tscherning et al. (1983);  
60 Wittwer et al. (2008). However, most of them, except Wittwer et al. (2008),

61 are restricted to a certain maximum degree of SHE (e.g. 2 700). In this pa-  
62 per, we present the novel MATLAB<sup>®</sup>-based graphical user interface (GUI)  
63 program for computing functionals of the geopotential up to an arbitrary  
64 degree and order. The outline of the paper is as follows: in section 2, the  
65 accuracy tests for the numerical evaluation of fnALFs using the three above  
66 mentioned approaches (i.e. the standard recursions, the modified recursions  
67 combined with Horner’s scheme and the extended-range arithmetic) are in-  
68 troduced. The SHS process, the lumped coefficients approach and the error  
69 propagation are described in this section as well. The developed software  
70 GrafLab and the numerical tests are introduced in section 3. In section 4,  
71 the contributions of the designed software and summary are presented.

## 72 2. Spherical harmonic synthesis

73 Let us start with the basic and well-known formula for the Earth’s exter-  
74 nal gravitational potential, expressed in the truncated series of the spherical  
75 harmonics (Hoffmann-Wellenhof and Moritz, 2005)

$$\begin{aligned}
V(r, \theta, \lambda) = & \frac{GM}{r} + \frac{GM}{r} \sum_{n=2}^M \left(\frac{R}{r}\right)^n \sum_{m=0}^n (\bar{C}_{nm} \cos m\lambda \\
& + \bar{S}_{nm} \sin m\lambda) \bar{P}_{nm}(\cos \theta),
\end{aligned} \tag{1}$$

76 in which  $GM$  is the geocentric gravitational constant of the Earth,  $R$  is  
77 the radius of the Earth,  $(r, \theta, \lambda)$  is the triplet of the spherical coordinates  
78 (spherical radius, spherical co-latitude and spherical longitude, respectively),  
79  $\bar{P}_{nm}(\cos \theta)$  are the fnALFs of degree  $n$  and order  $m$ ,  $\bar{C}_{nm}$  and  $\bar{S}_{nm}$  are the  
80 fully normalized spherical harmonic coefficients of degree  $n$  and order  $m$  and  
81  $M$  is the maximum degree of the SHE. Eq. (1) may be written in the form

82 of inverted summations over  $n$  and  $m$  as

$$\begin{aligned}
 V(r, \theta, \lambda) = & \frac{GM}{r} + \frac{GM}{r} \sum_{m=0}^M \left[ \cos m\lambda \sum_{n=\mu}^M \left(\frac{R}{r}\right)^n \bar{C}_{nm} \bar{P}_{nm}(\cos \theta) \right. \\
 & \left. + \sin m\lambda \sum_{n=\mu}^M \left(\frac{R}{r}\right)^n \bar{S}_{nm} \bar{P}_{nm}(\cos \theta) \right], \tag{2}
 \end{aligned}$$

83 where  $\mu$  is either 2 or  $m$ , whichever is the greater. If the fixed-degree re-  
 84 cursions have been used to compute fnALFs, Eq. (1) is more suitable, while  
 85 Eq. (2) should be used with the fixed-order recursions. In geodesy, Eq. (2)  
 86 and fixed-order recursions are usually preferred rather than Eq. (1) and fixed-  
 87 degree recursions.

88 In fact, Eq. (1) as well as Eq. (2) can be considered as the basic formulae  
 89 of SHS, from which an arbitrary functional of the geopotential can be derived,  
 90 see e.g. Barthelmes (2009).

91 *2.1. Numerical computation of the fully normalized associated Legendre func-*  
 92 *tions and their first- and second-order derivatives*

93 The numerical evaluation of fnALFs and their derivatives up to a high  
 94 degree is the most difficult part of the SHS. In the GrafLab, we used three  
 95 different approaches, which have been mentioned in section 1: (i) the stan-  
 96 dard forward column method (Holmes and Featherstone, 2002b); (ii) the  
 97 modified forward column method (ibid.); (iii) the extended-range arithmetic  
 98 (Fukushima, 2011). It is not the purpose of this paper to recapitulate here re-  
 99 cursions that can be found in many literature (Bosch, 2000; Colombo, 1981;  
 100 Fantino and Casotto, 2009; Fukushima, 2011, 2012; Holmes and Feather-  
 101 stone, 2002a,b). However, it should be mentioned that these recursions can

102 be modified by introducing the term  $(R/r)^n$  so that we finally get

$$\tilde{P}_{nm}(\cos \theta) = \left(\frac{R}{r}\right)^n \bar{P}_{nm}(\cos \theta), \quad (3)$$

103 which we name the modified fnALF. The main reason for doing this is that  
 104 the modified fnALFs may be evaluated directly during the recursions and  
 105 thus reduced the computation time of the whole SHS process, since large  
 106 matrix multiplications are eliminated. The reader can find more about this  
 107 approach e.g. in Bethencourt et al. (2005). In this section, we will focus on  
 108 the numerical stability of the recurrence relations used up to high and ultra-  
 109 high degrees. For this tests, the ordinary fnALFs instead of the modified  
 110 fnALFs were used.

111 In order to verify the numerical accuracy of computed fnALFs and their  
 112 derivatives, we used the accuracy test presented in Holmes and Featherstone  
 113 (2002b). Independently on the co-latitude, the following formulae must hold  
 114 (Fukushima, 2011, 2012)

$$I^{(0)} = \sum_{n=0}^M \sum_{m=0}^n \left(\bar{P}_{nm}^{(0)}(\cos \theta)\right)^2 = (M+1)^2, \quad \forall \theta, \quad (4a)$$

$$I^{(1)} = \sum_{n=0}^M \sum_{m=0}^n \left(\bar{P}_{nm}^{(1)}(\cos \theta)\right)^2 = \frac{M(M+2)(M+1)^2}{4}, \quad \forall \theta, \quad (4b)$$

$$I^{(2)} = \sum_{n=0}^M \sum_{m=0}^n \left(\bar{P}_{nm}^{(2)}(\cos \theta)\right)^2 = \left(\frac{M^2 + 2M - 1}{2}\right) I^{(1)}, \quad \forall \theta, \quad (4c)$$

117 wherein  $\bar{P}_{nm}^{(0)}(\cos \theta)$ ,  $\bar{P}_{nm}^{(1)}(\cos \theta)$  and  $\bar{P}_{nm}^{(2)}(\cos \theta)$  denote the zero-, first- and  
 118 second-order derivatives of fnALFs with respect to the spherical co-latitude,  
 119 respectively. The identity error is then given as

$$\delta I^{(d)} = \left| \frac{I_{\text{computed}}^{(d)}}{I_{\text{theoretical}}^{(d)}} - 1 \right|, \quad (5)$$

120 where  $d = 0, 1, 2$  denotes the order of the derivatives of fnALFs. Note that in  
 121 the case of the modified forward column method, the scaled values of fnALFs  
 122 or their derivatives must be combined with Horner's scheme, see Holmes and  
 123 Featherstone (2002b).

124 The values of  $\bar{P}_{nm}^{(d)}(\cos \theta)$  range over thousands of orders of magnitude and  
 125 therefore cannot be squared (see Eqs. (4a)-(4c)) in double precision due to  
 126 the under-flow and over-flow problems. Hence, these values were computed  
 127 in double precision using the above mentioned approaches, subsequently they  
 128 were converted to quadruple precision and finally, squared and summed in  
 129 quadruple precision. However, MATLAB<sup>®</sup> does not support the quadruple  
 130 precision, thus, these algorithms were rewritten into Fortran 90, compiled by  
 131 the Intel Visual Fortran Composer XE 2011 and executed at a computer with  
 132 2.5 GHz dual-core CPU and 3 GB RAM under the 32 bit Windows 7 OS. The  
 133 routines used for computing fnALFs using the extended-range arithmetic,  
 134 written in Fortran 90, are available from Fukushima (2011). These routines  
 135 were rewritten into the MATLAB<sup>®</sup> and used in the GrafLab software.

136 Based on our numerical accuracy tests, the three above mentioned ap-  
 137 proaches may be used up to the following maximum degrees:

- 138 (i) the standard forward column method:  $M_{\max} = 1\ 800$ ,
- 139 (ii) the modified forward column method:  $M_{\max} = 2\ 700$ ,
- 140 (iii) the extended-range arithmetic: up to an arbitrary degree.

141 These statements are supported by Figures A.1 - A.3, which represent the  
 142 base-10 logarithm of the identity errors  $\delta I^{(d)}$  computed for all integer values  
 143 of co-latitudes  $0^\circ \leq \theta \leq 90^\circ$  in the case of  $d = 0$  and  $0^\circ < \theta \leq 90^\circ$  if  
 144  $d = 1, 2$ . Note that the recurrence relations used for evaluating the first- and

145 second-order derivatives of fnALFs are singular at poles (Fukushima, 2012,  
 146 Appendix A.1).

147 Figure A.1 should be positioned here

148 Figure A.2 should be positioned here

149 Figure A.3 should be positioned here

150 Furthermore, inspection of Figure A.4 shows that the standard forward  
 151 column method may also be used up to degree  $M = 2190$ , but only for  
 152 the co-latitudes  $\theta \in \langle 0^\circ, 10^\circ \rangle \cup \langle 34^\circ, 90^\circ \rangle$  in the case of fnALFs and  $\theta \in$   
 153  $\langle 0^\circ, 10^\circ \rangle \cup \langle 34^\circ, 90^\circ \rangle$  in the case of their derivatives. The computational labor  
 154 of this approach is the lowest, therefore this approach should be applied if  
 155 possible. We will focus on the time-efficiency of these three approaches in  
 156 section 3.2.

157 Figure A.4 should be positioned here

### 158 2.2. Lumped coefficients approach

159 When applying Eq. (2) on a regular grid, it may be rewritten into a  
 160 much efficient form. Both summation, i.e. the summation over  $n$  and sub-  
 161 sequently over  $m$ , can be done by matrix multiplications using the lumped  
 162 coefficients, sometimes called the Fourier coefficients. In Eq. (2), the terms  
 163  $\sum_{n=\mu}^M (R/r)^n \overline{C}_{nm} \overline{P}_{nm}(\cos \theta)$  and  $\sum_{n=\mu}^M (R/r)^n \overline{S}_{nm} \overline{P}_{nm}(\cos \theta)$  are constant  
 164 for each meridian in the grid and therefore no need to be computed more  
 165 than once. With this in mind, Eq. (2) may be written in the matrix form as

$$\mathbf{V} = (GM \odot \mathbf{r}) \odot \left[ 1 + \left( \mathbf{A}(\boldsymbol{\theta}) \cdot \cos(\mathbf{m} \cdot \boldsymbol{\lambda}) + \mathbf{B}(\boldsymbol{\theta}) \cdot \sin(\mathbf{m} \cdot \boldsymbol{\lambda}) \right) \right], \quad (6)$$

166 in which  $\mathbf{A}_{N_\theta \times (M+1)}(\boldsymbol{\theta})$  and  $\mathbf{B}_{N_\theta \times (M+1)}(\boldsymbol{\theta})$  are the matrices of the lumped co-  
 167 efficients, where  $N_\theta$  denotes the number of the points in one meridian,  $\mathbf{r}_{N_\theta \times N_\lambda}$   
 168 is the matrix of the spherical radii of every point in the grid,  $N_\lambda$  denotes the  
 169 number of the points in one latitude parallel,  $\boldsymbol{\theta}_{N_\theta \times 1}$  is the column vector of  
 170 the spherical co-latitudes,  $\boldsymbol{\lambda}_{1 \times N_\lambda}$  is the row vector of the spherical longitudes  
 171 and  $\mathbf{m}_{(M+1) \times 1}$  is the column vector with the structure  $\mathbf{m} = [0 \ 1 \ \dots \ M]^\top$ .  
 172 The symbol  $\odot$  denotes the Hadamard product (Grafarend, 2006), which may  
 173 be used for the matrices of the same dimensions in order to multiply each  
 174 corresponding elements of the matrices (element-wise product), while the  
 175 symbol  $\cdot$  denotes the Cayley product (matrix product) (ibid.). We also in-  
 176 troduced the symbol  $\oslash$ , which denotes an element-wise division of a scalar  
 177 (or a matrix) by a matrix. In fact, in Eq. (6) only the vector  $\mathbf{r}_{N_\theta \times 1}$  is needed  
 178 instead of the matrix  $\mathbf{r}_{N_\theta \times N_\lambda}$ , and each column of the matrix in the square  
 179 brackets in Eq. (6) may be multiplied using the Hadamard product by the  
 180 vector  $\mathbf{r}_{N_\theta \times 1}$ , so there is no need to store the redundant data. In MATLAB<sup>®</sup>,  
 181 the built-in function `bsxfun`<sup>®</sup> is designed for this purpose. However, for the  
 182 sake of clarity we used this notation in the whole paper, but in the GrafLab,  
 183 the `bsxfun`<sup>®</sup> function was used.

184 The vectors of the lumped coefficients of order  $m$  are defined as

$$\left. \begin{array}{l} \mathbf{A}_m(\boldsymbol{\theta}) \\ \mathbf{B}_m(\boldsymbol{\theta}) \end{array} \right\} = \tilde{\mathbf{P}}_m \cdot \left\{ \begin{array}{l} \bar{\mathbf{C}}_m \\ \bar{\mathbf{S}}_m \end{array} \right. \quad (7)$$

185 where  $\tilde{\mathbf{P}}_m$  is the matrix of the modified fnALFs with the structure

$$\tilde{\mathbf{P}}_m = \begin{bmatrix} \tilde{P}_{m,m}(\cos \theta_1) & \tilde{P}_{m+1,m}(\cos \theta_1) & \cdots & \tilde{P}_{M,m}(\cos \theta_1) \\ \tilde{P}_{m,m}(\cos \theta_2) & \tilde{P}_{m+1,m}(\cos \theta_2) & \cdots & \tilde{P}_{M,m}(\cos \theta_2) \\ \vdots & \vdots & \ddots & \vdots \\ \tilde{P}_{m,m}(\cos \theta_{N_\theta}) & \tilde{P}_{m+1,m}(\cos \theta_{N_\theta}) & \cdots & \tilde{P}_{M,m}(\cos \theta_{N_\theta}) \end{bmatrix} \quad (8)$$

186 and

$$\bar{\mathbf{C}}_m = [\bar{C}_{m,m} \quad \bar{C}_{m+1,m} \quad \cdots \quad \bar{C}_{M,m}]^\top, \quad (9a)$$

187

$$\bar{\mathbf{S}}_m = [\bar{S}_{m,m} \quad \bar{S}_{m+1,m} \quad \cdots \quad \bar{S}_{M,m}]^\top. \quad (9b)$$

188 Finally, we obtain the full matrices of the lumped coefficients

$$\mathbf{A}(\boldsymbol{\theta}) = [\mathbf{A}_{m=0}(\boldsymbol{\theta}) \quad \mathbf{A}_{m=1}(\boldsymbol{\theta}) \quad \cdots \quad \mathbf{A}_{m=M}(\boldsymbol{\theta})], \quad (10a)$$

189

$$\mathbf{B}(\boldsymbol{\theta}) = [\mathbf{B}_{m=0}(\boldsymbol{\theta}) \quad \mathbf{B}_{m=1}(\boldsymbol{\theta}) \quad \cdots \quad \mathbf{B}_{m=M}(\boldsymbol{\theta})]. \quad (10b)$$

190 Using this approach, an arbitrary functional of the geopotential can be  
 191 evaluated on a regular grid much faster than using the point-wise approach  
 192 with two loops, one degree-depended and one order-depended. In fact, the  
 193 factor of increased computational speed is of several thousands, which is  
 194 remarkable.

### 195 *2.3. Error propagation*

196 In general, the spherical harmonic coefficients are estimated by the least  
 197 squares method using terrestrial and/or satellite measurements, which are  
 198 not errorless. The least squares method enables to estimate the full variance-  
 199 covariance matrix of these coefficients as well. When computing an arbitrary

200 functional of the geopotential using these estimated coefficients, their er-  
 201 rors are propagated to the functional obeying the error variance-covariance  
 202 propagation law (Grafarend, 2006). This error is known as the commission  
 203 error. For the linear transformation of the variance-covariance matrix of  
 204 the spherical harmonic coefficients to the variance-covariance matrix of the  
 205 gravitational potential the following formula may be written

$$\mathbf{\Sigma}_V = \mathbf{A} \cdot \mathbf{\Sigma}_{\text{SHC}} \cdot \mathbf{A}^\top, \quad (11)$$

206 where  $\mathbf{\Sigma}_{\text{SHC}}$  is the variance-covariance matrix of the spherical harmonic co-  
 207 efficients with the structure

$$\mathbf{\Sigma}_{\text{SHC}} = \begin{bmatrix} v_{20,20}^{CC} & c_{20,30}^{CC} & \cdots & c_{20,M0}^{CC} & c_{20,21}^{CC} & c_{20,21}^{CS} & c_{20,31}^{CC} & \cdots & c_{20,MM}^{CS} \\ c_{30,20}^{CC} & v_{30,30}^{CC} & \cdots & c_{30,M0}^{CC} & c_{30,21}^{CC} & c_{30,21}^{CS} & c_{30,31}^{CC} & \cdots & c_{30,MM}^{CS} \\ \vdots & \vdots & \ddots & \vdots & \vdots & \vdots & \vdots & \cdots & \vdots \\ c_{M0,20}^{CC} & c_{M0,30}^{CC} & \cdots & v_{M0,M0}^{CC} & c_{M0,21}^{CC} & c_{M0,21}^{CS} & c_{M0,31}^{CC} & \cdots & c_{M0,MM}^{CS} \\ c_{21,20}^{CC} & c_{21,30}^{CC} & \cdots & c_{21,M0}^{CC} & v_{21,21}^{CC} & v_{21,21}^{CS} & v_{21,31}^{CC} & \cdots & v_{21,MM}^{CS} \\ c_{21,20}^{SC} & c_{21,30}^{SC} & \cdots & c_{21,M0}^{SC} & c_{21,21}^{SC} & v_{21,21}^{SS} & v_{21,31}^{SC} & \cdots & v_{21,MM}^{SS} \\ c_{31,20}^{CC} & c_{31,30}^{CC} & \cdots & c_{31,M0}^{CC} & c_{31,21}^{CC} & c_{31,21}^{CS} & v_{31,31}^{CC} & \cdots & c_{31,MM}^{CS} \\ \vdots & \vdots & \cdots & \vdots & \vdots & \vdots & \vdots & \ddots & \vdots \\ c_{MM,20}^{SC} & c_{MM,30}^{SC} & \cdots & c_{MM,M0}^{SC} & c_{MM,21}^{SC} & c_{MM,21}^{SS} & c_{MM,31}^{SC} & \cdots & v_{MM,MM}^{SS} \end{bmatrix}, \quad (12)$$

208 where  $v_{20,20}^{CC}$  denotes the variance of the coefficient  $\overline{C}_{20}$ ,  $c_{20,21}^{CS}$  is the covariance  
 209 between the coefficients  $\overline{C}_{20}$  and  $\overline{S}_{21}$ , etc., and  $\mathbf{A}$  is the design matrix of  
 210 the partial derivatives of Eq. (2) with respect to the individual spherical  
 211 harmonic coefficients. Note that the partial derivatives in the matrix  $\mathbf{A}$  must  
 212 correspond to the organization of the individual elements in the matrix  $\mathbf{\Sigma}_{\text{SHC}}$ .  
 213 Since the structure of the matrix  $\mathbf{\Sigma}_{\text{SHC}}$  has not yet been standardized, only  
 214 this particular structure of the variance-covariance matrix, which is probably  
 215 the most common, can be recognized by the GrafLab. Finally, the square

216 roots of the diagonal elements of the matrix  $\Sigma_{\mathbf{V}}$  represent the commission  
217 errors of the gravitational potential in the particular computing points.

218 Note that the matrix  $\Sigma_{\text{SHC}}$  of a GGM may or may not be calibrated.  
219 If the matrix  $\Sigma_{\text{SHC}}$  is calibrated, the computed commission errors may be  
220 considered as real. If this matrix is not calibrated, the evaluated commission  
221 errors must be considered only as a relative indicator of accuracy of the GGM  
222 in a certain area on the globe with respect to another area.

### 223 **3. Software presentations**

#### 224 *3.1. Description of the software*

225 In this section, we will describe in detail the created software GrafLab  
226 (GRAvity Field LABoratory) and the basic principles of manipulation with  
227 the software. The source code of the GrafLab, as well as its graphical user  
228 interface (GUI), have been written in MATLAB<sup>®</sup>. The GUI, see Figure A.5,  
229 allows comfortable and intuitive manipulation with all functionalities of the  
230 software.

231 Figure A.5 should be positioned here

232 The GUI of the application is visually divided into three panels:

233 (i) *Geopotential model and reference system selection*: At first, the input  
234 GGM file or its error variance-covariance matrix must be imported using the  
235 *Browse...* button. The input GGM file must have one of the two standard-  
236 ized structures, see Table A.1 and Table A.2. Only this two structures can  
237 be recognized by the GrafLab. In addition to the spherical harmonic coeffi-  
238 cients, the input file may or may not contains the fifth and the sixth column

239 with their standard deviations. The input file may either be an ASCII file  
240 or a binary MAT-file. In case of the GGM with a high maximum degree of  
241 SHE, it is recommended to use the binary MAT-file, since it can be loaded  
242 much faster.

243 Table A.1 should be positioned here

244 Table A.2 should be positioned here

245 The input ASCII file of error variance-covariance matrix must have the  
246 structure as shown in the Table A.3. A binary MAT-file may be used to  
247 import error variance-covariance matrix as well. However, in this case, the  
248 empty arrays in Table A.3 must be filled with zeroes or corresponding co-  
249 variances.

250 Table A.3 should be positioned here

251 Most of GGMs have the same values of the geocentric gravitational con-  
252 stant and the radius of the Earth, therefore in this panel GrafLab automat-  
253 ically offers these values for the computation. However, they may be simply  
254 replaced by the required values, if necessary. The  $n_{\min}$  value of SHE is implic-  
255 itly set to 2 and cannot be changed, unlike the value of  $n_{\max}$ . Only integer  
256 values of  $n_{\max}$  in the interval  $n_{\max} \in \langle 2, M \rangle$  are accepted. From the pop-  
257 up menu *Ellipsoid*, the normal gravity field generated by the equipotential  
258 ellipsoid WGS84 (NIMA, 2000) or GRS80 (Moritz, 2000) can be selected.

259 (ii) *Point type selection*: In the point type selection panel, one of three or-  
260 ganizations of the evaluation points must be specified by selecting the check-  
261 box: *Grid*, *Load data* or *Point-wise*. If the grid is selected, the minimum,

262 maximum and discretization step in the ellipsoidal latitude and ellipsoidal  
263 longitude directions must be entered. The array  $h$  ( $m$ ) denotes the constant  
264 ellipsoidal height of the grid above the reference ellipsoid. For the com-  
265 putation on a regular grid, the lumped coefficients approach described in  
266 section 2.2 is used.

267 To import the computational points from a data file, the *Load data* check-  
268 box must be selected and subsequently, the data file must be imported using  
269 the *Browse...* button next to the checkbox. The data file may contain es-  
270 sentially an arbitrary number of lines and in every line of the file, the triplet  
271 of the ellipsoidal coordinates (ellipsoidal latitude, ellipsoidal longitude and  
272 ellipsoidal height) must be given.

273 After selecting the checkbox *Point-wise*, an arbitrary point defined also  
274 by the triplet of the ellipsoidal coordinates can be entered manually using the  
275 arrays  $phi$  ( $^\circ$ ),  $lambda$  ( $^\circ$ ),  $h$  ( $m$ ). In case of several points, the coordinates  
276 in each array must be separated by the comma or by the space. This point  
277 type selection is suitable if only a few points are to be determined, so there  
278 is no need to create a data file to import.

279 In the last two mentioned cases of the point type selection, the lumped  
280 coefficients approach cannot be applied due to irregular distribution of the  
281 points. Therefore we used two loops, one degree-dependent and one order-  
282 dependent, and programmed the routines for computing all functionals as it  
283 is shown in Eq. (2).

284 In each of the three above mentioned point type selections, the entries  
285 must be either in the form of floating point numbers with decimal dots or  
286 integer values.

287 (iii) *Calculated parameters and output selection*: Using the four pop-up  
 288 menus on the left side of this panel, user can simply choose, which func-  
 289 tionals of the geopotential are to be computed. Note that at least one and  
 290 maximum four functionals may be computed simultaneously. GrafLab per-  
 291 mits to compute the following functionals of the geopotential (the value in  
 292 the superscript denotes the level of computational demand; (1) is small, (2)  
 293 is medium and (3) is high): gravitational potential  $V^{(1)}$ , diagonal compo-  
 294 nents of the gravitational tensor in the spherical coordinates  $V_{rr}^{(3)}, V_{\theta\theta}^{(3)}, V_{\lambda\lambda}^{(3)}$ ,  
 295 non-diagonal components of the gravitational tensor in the spherical coor-  
 296 dinates  $V_{r\theta}^{(3)}, V_{r\lambda}^{(3)}, V_{\theta\lambda}^{(3)}$ , diagonal components of the gravitational tensor in  
 297 the local north-oriented frame (LNOF)  $V_{xx}^{(2)}, V_{yy}^{(2)}, V_{zz}^{(2)}$ , non-diagonal compo-  
 298 nents of the gravitational tensor in the LNOF  $V_{xy}^{(3)}, V_{xz}^{(3)}, V_{yz}^{(3)}$ , gravity po-  
 299 tential  $W^{(1)}$ , gravity  $g^{(2)}$ , gravity in spherical approximation  $g_{sa}^{(1)}$ , second  
 300 radial derivative of gravity potential  $W_{rr}^{(1)}$ , disturbing potential  $T^{(1)}$ , grav-  
 301 ity disturbance  $\delta g^{(2)}$ , gravity disturbance in spherical approximation  $\delta g_{sa}^{(1)}$ ,  
 302 gravity anomaly in spherical approximation  $\Delta g_{sa}^{(1)}$ , second radial derivative  
 303 of disturbing potential  $T_{rr}^{(1)}$ , diagonal components of the disturbing tensor  
 304 in the spherical coordinates  $T_{rr}^{(3)}, T_{\theta\theta}^{(3)}, T_{\lambda\lambda}^{(3)}$ , non-diagonal components of the  
 305 disturbing tensor in the spherical coordinates  $T_{r\theta}^{(3)}, T_{r\lambda}^{(3)}, T_{\theta\lambda}^{(3)}$ , diagonal compo-  
 306 nents of the disturbing tensor in the LNOF  $T_{xx}^{(2)}, T_{yy}^{(2)}, T_{zz}^{(2)}$ , non-diagonal  
 307 components of the disturbing tensor in the LNOF  $T_{xy}^{(3)}, T_{xz}^{(3)}, T_{yz}^{(3)}$ , north-south  
 308 component of the deflection of the vertical  $\xi^{(2)}$ , east-west component of the  
 309 deflection of the vertical  $\eta^{(1)}$ , total deflection of the vertical  $\Theta^{(2)}$ , geoid un-  
 310 dulation  $N^{(2)}$ , generalized height anomaly  $\zeta_{Ell}^{(1)}$ , height anomaly  $\zeta^{(2)}$ . In or-  
 311 der to stay brief, we do not introduce here the mathematical formulae for

312 computing each functional, but these can be found in the pdf file Defini-  
313 tion\_of\_functionals\_of\_the\_geopotential\_used\_in\_GrafLab\_software.pdf available  
314 at <sup>1</sup>. For evaluating disturbing and gravitational tensor in the LNOF, we used  
315 the non-singular expressions, which can be found e.g. in Petrovskaya and Ver-  
316 shkov (2006). For practical reasons, we slightly modified these formulae, see  
317 Appendix A.

318 To compute geoid undulation  $N$  and height anomaly  $\zeta$ , the digital terrain  
319 model, e.g. DTM2006.0 (Pavlis et al., 2007), must be imported. Only one  
320 particular structure of the DTM file, shown in Table A.1, can be recognized  
321 by the GrafLab. If these two functionals are to be computed, immediately  
322 after clicking the *OK* button, the dialog window from which the input DTM  
323 file must be imported will appear.

324 Each functional of the geopotential may be evaluated using any of the  
325 three mentioned approaches for computing fnALFs except for the gravita-  
326 tional and disturbing tensors in the LNOF. Since these non-singular expres-  
327 sions have been slightly modified, the modified forward column method com-  
328 bined with Horner's scheme is not efficient for the new formulae and therefore  
329 it was not used in this case.

330 In order to evaluate the commission errors of the functionals, the *Com-*  
331 *mission error* check box must be selected. GrafLab allows to compute the  
332 commission errors (see section 2.3) of the each above mentioned functional ex-  
333 cept for the gravitational and disturbing tensors in the LNOF:  $T_{xx}, T_{yy}, T_{zz};$   
334  $T_{xy}, T_{xz}, T_{yz}; V_{xx}, V_{yy}, V_{zz}; V_{xy}, V_{xz}, V_{yz}$ . One should keep in mind that the

---

<sup>1</sup>[http://www.svf.stuba.sk/en/departments/departments-of-theoretical-geodesy/science-and-research/downloads.html?page\\_id=4996](http://www.svf.stuba.sk/en/departments/departments-of-theoretical-geodesy/science-and-research/downloads.html?page_id=4996)

335 evaluation of commission error has much higher requirements on the com-  
336 puter, because of the large size of the matrix  $\Sigma_{\text{SHC}}$ . In practice it means  
337 that the maximum degree  $M$  must be reduced from thousands or hundreds  
338 to tens, and number of computing points have to be decreased as well.

339 By clicking the button *Computation of fnALFs*, a new dialog window will  
340 appear, see Figure A.6, in which user may choose one of the three approaches  
341 for evaluating values of fnALFs (see section 2.1).

342 Figure A.6 should be positioned here

343 The computed data may be depicted on a map using automatically se-  
344 lected cartographic projection. By clicking the button *Display data settings*,  
345 another dialog window illustrated by Figure A.7 will appear. Here, user can  
346 set up the required output parameters of the exported map. This option is  
347 available only if the computation on a regular grid has been chosen. Demon-  
348 strations of exported maps are shown in Figure A.8 and Figure A.9.

349 Figure A.7 should be positioned here

350 Figure A.8 should be positioned here

351 Figure A.9 should be positioned here

352 The button *Output folder and file* permits to specify the output folder  
353 and prefix of the all exported files, i.e. without any suffix (e.g. Prefix).  
354 The data file (e.g. Prefix.txt) with the computed data may be created by  
355 selecting the checkbox *Export data*. The report file, which contains the infor-  
356 mations about the computation, see Table A.4, may be created by selecting

357 the *Export report* checkbox. This file automatically obtains name with the  
358 suffix `_Report.txt`, e.g. `Prefix_Report.txt`. If the *Display data* checkbox has  
359 been selected, GrafLab creates also a graphical file (or files, depending on  
360 the number of computing functionals) according to chosen graphic file format  
361 (bmp, emf, eps, jpeg, pdf, png or tiff).

362 Table A.4 should be positioned here

363 When all the required input parameters and input files have been entered,  
364 after clicking the *OK* button, the computation will start. On the left from  
365 this button, there is a status line, which provides short explanations during  
366 the whole computational process (*Loading GGM file...*, current value of the  
367 variable  $m$  in the order-dependent loop, *Displaying data...*, ...), so one can  
368 clearly see in which part of the computation is GrafLab. After successful  
369 computation, the status *Computation has been finished* will appear. If any  
370 of the input parameters or input files have been entered in a wrong format,  
371 GrafLab will open a warning dialog or error dialog with description of the  
372 error.

373 The whole source code of the program called `GrafLab.m` is written as  
374 a one function. It contains approximately 8 000 lines of the source code,  
375 therefore in Figure A.10 we provide a simple flowchart of the program, so  
376 one can clearly see its structure.

377 Figure A.10 should be positioned here

378 *3.2. Testing of the software*

379 In this section, we focus on the efficiency of the algorithms used in the  
380 GrafLab. We performed two separate tests, one for the lumped coefficients  
381 approach (computation on a regular grid) and the second for the point-wise  
382 approach (computation on irregularly distributed points). In each exper-  
383 iment we tested the time-efficiency of all three approaches for computing  
384 values of fnALFs in the context of SHS. For these tests we chose two func-  
385 tionals: disturbing potential and disturbing tensor in the LNOF (diagonal  
386 and off-diagonal elements separately). All numerical experiments were per-  
387 formed on an ordinary computer with 2.5 GHz dual-core CPU and 3 GB  
388 RAM under the 32 bit Windows 7 OS.

389 In Figure A.11 and Figure A.12 we plot the CPU time for computing  
390 disturbing potential using  $M = 360$  and  $M = 2\ 190$ , respectively, on a  
391 global grid versus different grid resolution. The same numerical tests using  
392 disturbing tensor are illustrated in Figure A.13 and Figure A.14. Note that  
393 the standard forward column method should not be applied on a global grid  
394 if  $M > 1\ 800$ , see Figure A.4. However, in order to assess the time-efficiency  
395 of the algorithm only, it was used.

396 Figure A.11 should be positioned here

397 Figure A.12 should be positioned here

398 Figure A.13 should be positioned here

399 Figure A.14 should be positioned here

400 Figure A.13 and Figure A.14 reveal that all gravity gradients in the LNOF

401 (i.e. diagonal and off-diagonal elements of the tensor) can be synthesized on  
402 a global grid  $5' \times 5'$  within 74 s if  $M = 360$  and on a global grid  $10' \times 10'$   
403 within 936 s if  $M = 2\,190$ .

404 Similar tests, see Figures A.15 - A.18, were done for the point-wise ap-  
405 proach, in which we used the computational points randomly distributed on  
406 the globe.

407 Figure A.15 should be positioned here

408 Figure A.16 should be positioned here

409 Figure A.17 should be positioned here

410 Figure A.18 should be positioned here

411 As expected, the point-wise approach is significantly more time-consuming  
412 than the lumped coefficients approach. Hence, for a high maximum degree  
413 (e.g.  $M = 2\,190$ ) we recommend to use this approach for tens of thousands  
414 of computation points at most.

415 In general, from Figures A.11 - A.18 it is seen that the SHS with fnALFs  
416 evaluated using the extended-range arithmetic takes only approximately 2-3  
417 times longer than using the standard forward column method. Furthermore,  
418 for a large data set on a grid and maximum degrees ranging from 1 801 to  
419 2 700, it is much more effective to use the extended-range arithmetic than the  
420 modified forward column method. In contrast, in the point-wise approach  
421 and maximum degrees in the same interval, the modified forward column  
422 method should be preferred rather than the extended-range arithmetic, since  
423 it required significantly less computation time.

424 As mentioned, the tests were performed on a 32 bit version of MATLAB<sup>®</sup>  
425 and Windows 7 OS. However, on a 64 bit architecture we found the algo-  
426 rithm for computing fnALFs using extended-range arithmetic extremely slow.  
427 Thus, to make this algorithm more effective on this architecture, we slightly  
428 modified the program in order to speed up the extended-range arithmetic  
429 approach. However, on a 64 bit version of MATLAB<sup>®</sup> the extended-range  
430 arithmetic approach still remains 8-10 times slower than the standard forward  
431 column method. During the computation, GrafLab automatically identifies  
432 the bit architecture of MATLAB<sup>®</sup> on which the computation is performed  
433 and uses the appropriate version of the algorithm.

#### 434 **4. Summary**

435 In this paper, we have been presented a new MATLAB<sup>®</sup>-based graphical  
436 user interface program for spherical harmonic synthesis. GrafLab allows  
437 to easily compute and depict 18 various functionals of the geopotential as  
438 well as their commission errors. Fully normalized ALFs may be obtained  
439 using three different approaches from which one approach enables to evaluate  
440 the fnALFs up to an arbitrary degree and order in the cost of only 2-3  
441 times increased computation time compared with the standard algorithms.  
442 A modified non-singular expressions for the gravity gradients in the LNOF  
443 have been introduced as well.

444 The main advantages of the GrafLab are that it is not restricted to a  
445 maximum degree of SHE essentially, it is fast, versatile and simple for usage  
446 through an intuitive and comfortable GUI. The primary exploitation of the  
447 GrafLab is supposed to be in scientific tasks related to the spherical harmonic

448 synthesis of functionals of the geopotential. Since the program is controlled  
 449 through a convenient GUI, it may be used as an efficient tool for educational  
 450 purposes as well.

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 455 manuscript.

### 456 **Appendix A. Modified non-singular expressions for the gravity** 457 **gradients in the LNOF**

458 The used non-singular expressions for the gravity gradients in the LNOF  
 459 can be found e.g. in Petrovskaya and Vershkov (2006). We will not reca-  
 460 pitulate here all those formulae. As an example, let us mentioned only one  
 461 particular expression for the element  $T_{xx}$ , which has the following form

$$\begin{aligned}
 T_{xx} = & \frac{GM}{r^3} \sum_{n=2}^M \left(\frac{R}{r}\right)^n \sum_{m=0}^n (\bar{C}_{nm} \cos m\lambda + \bar{S}_{nm} \sin m\lambda) \\
 & \times \left( a_{nm} \bar{P}_{n,m-2}(\cos \theta) \right. \\
 & + [b_{nm} - (n+1)(n+2)] \bar{P}_{nm}(\cos \theta) \\
 & \left. + c_{nm} \bar{P}_{n,m+2}(\cos \theta) \right), \tag{A.1}
 \end{aligned}$$

462 in which

$$a_{nm} = 0, \quad m = 0, 1 \tag{A.2}$$

463

$$a_{nm} = \frac{\sqrt{1 + \delta_{m,2}}}{4} \sqrt{n^2 - (m-1)^2} \times \sqrt{n+m} \sqrt{n-m+2}, \quad 2 \leq m \leq n \quad (\text{A.3})$$

464

$$b_{nm} = \frac{(n+m+1)(n+m+2)}{2(m+1)}, \quad m = 0, 1 \quad (\text{A.4})$$

465

$$b_{nm} = \frac{n^2 + m^2 + 3n + 2}{2}, \quad 2 \leq m \leq n \quad (\text{A.5})$$

466

$$c_{nm} = \frac{\sqrt{1 + \delta_{m,0}}}{4} \sqrt{n^2 - (m+1)^2} \sqrt{n-m} \times \sqrt{n+m+2}, \quad m = 0, 1 \quad (\text{A.6})$$

467

$$c_{nm} = \frac{1}{4} \sqrt{n^2 - (m+1)^2} \sqrt{n-m} \sqrt{n+m+2}, \quad 2 \leq m \leq n \quad (\text{A.7})$$

468

$$\delta_{p,q} = \begin{cases} 1, & p = q, \\ 0, & p \neq q. \end{cases} \quad (\text{A.8})$$

469 From Eq. (A.1), one can see that in addition to the term  $\bar{P}_{nm}(\cos \theta)$ , two  
470 other terms  $\bar{P}_{n,m-2}(\cos \theta)$  and  $\bar{P}_{n,m+2}(\cos \theta)$  must be computed for each  $m$ .  
471 From the practical numerical point of view, this is not an issue, if fixed-degree  
472 recursions have been used to evaluate fnALFs. In this case, for each  $m$  these  
473 terms have been already computed with the term  $\bar{P}_{nm}(\cos \theta)$  essentially. In  
474 the GrafLab, however, we used fixed-order recursions, which are preferred in  
475 geodesy. In this case, with every change of  $m$  in the order-dependent loop, it  
476 is necessary to evaluate not only the term  $\bar{P}_{nm}(\cos \theta)$ , but also the two other  
477 terms. Another words, redundant computations occur. Thus, we modified  
478 Eq. (A.1) in the way that only the term  $\bar{P}_{nm}(\cos \theta)$  is needed to be computed.

479 We present Eq. (A.1) in the following form

$$\begin{aligned}
T_{xx} = & \frac{GM}{r^3} \sum_{n=2}^M \left(\frac{R}{r}\right)^n \\
& \times \sum_{m=0}^n \left[ (\bar{C}_{n,m+2} \cos(m+2)\lambda + \bar{S}_{n,m+2} \sin(m+2)\lambda) a_{n,m+2} \right. \\
& + (\bar{C}_{nm} \cos m\lambda + \bar{S}_{nm} \sin m\lambda) (b_{nm} - (n+1)(n+2)) \\
& \left. + (\bar{C}_{n,m-2} \cos(m-2)\lambda + \bar{S}_{n,m-2} \sin(m-2)\lambda) c_{n,m-2} \right] \\
& \times \bar{P}_{nm}(\cos \theta),
\end{aligned} \tag{A.9}$$

480 where

$$\left. \begin{array}{l} \bar{C}_{n,m+2} \\ \bar{S}_{n,m+2} \\ \cos(m+2)\lambda \\ \sin(m+2)\lambda \\ a_{n,m+2} \end{array} \right\} = 0, \quad m+2 > n, \tag{A.10}$$

481

$$\left. \begin{array}{l} \bar{C}_{n,m-2} \\ \bar{S}_{n,m-2} \\ \cos(m-2)\lambda \\ \sin(m-2)\lambda \\ c_{n,m-2} \end{array} \right\} = 0, \quad m-2 < 0. \tag{A.11}$$

482 The main idea of Eq. (A.9) is that the set of spherical harmonic co-  
483 efficients is usually stored during the whole computational process, hence  
484 the coefficients  $\bar{C}_{n,m+2}, \bar{S}_{n,m+2}$  and  $\bar{C}_{n,m-2}, \bar{S}_{n,m-2}$  may be simply restored  
485 when necessary instead of the redundant computation of  $\bar{P}_{n,m-2}(\cos \theta)$  and

486  $\bar{P}_{n,m+2}(\cos \theta)$  in Eq. (A.1). The formulae for the remaining elements  $T_{yy}, T_{zz}, T_{xy}, T_{xz}, T_{yz}$   
487 may be easily modified in the same way.

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589 column method (maximum degree:  $M = 1\,800$ ; *solid line*);  
590 (ii) the modified forward column method (maximum degree:  
591  $M = 2\,700$ ; *dotted line*); (iii) the extended-range arithmetic  
592 (maximum degree:  $M = 65\,536$ ; *dashed line*). . . . . 41

593 A.4 Base-10 logarithm of the identity errors  $\delta I^{(0)}$ ,  $\delta I^{(1)}$ ,  $\delta I^{(2)}$  of the  
594 zero-, first- and second-order derivatives of fnALFs, respec-  
595 tively, using the standard forward column method (maximum  
596 degree:  $M = 2\,190$ ;  $\delta I^{(0)}$  – *solid line*;  $\delta I^{(1)}$  – *dotted line*;  $\delta I^{(2)}$   
597 – *dashed line*). . . . . 42

598 A.5 GrafLab graphical user interface. . . . . 43

599	A.6	Computation of fnALFs window. . . . .	44
600	A.7	Display data settings window. . . . .	45
601	A.8	Geoid undulation computed and depicted using the GrafLab	
602		software. The geoid undulation is computed on the regular	
603		grid $\varphi \in \langle 35^\circ, 75^\circ \rangle$ , $\lambda \in \langle -15^\circ, 35^\circ \rangle$ with spatial resolution	
604		$0.1^\circ$ using EGM2008 and DTM2006.0 (maximum degree of	
605		SHE: $M = 2\ 190$ ). . . . .	46
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607		using the GrafLab software. The commission errors of geoid	
608		undulation are computed on the regular grid $\varphi \in \langle -90^\circ, 90^\circ \rangle$ ,	
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610		variance-covariance matrix of GRIM5C1 (maximum degree of	
611		SHE: $M = 70$ ; the error variance-covariance matrix is not	
612		calibrated). . . . .	47

613 A.10 Flowchart of the GrafLab. Explanation of the symbols and  
614 abbreviations in the flowchart:  $\varphi, \lambda, h$ , GGM – ellipsoidal co-  
615 ordinates of the evaluation points, global geopotential model  
616 of the Earth; Error check 1 – the first error check of the input  
617 data; DTM – digital terrain model; Error check 2 – the second  
618 error check of the input data; Grid, Load data, Point-wise –  
619 point type selection; SFCM, MFCM, ERA – computation of  
620 the fnALFs using the standard forward column method, the  
621 modified forward column method or the extended-range arith-  
622 metic approach, respectively; dmfnALFs – computation of the  
623 first-order derivatives of the modified fnALFs; ddmfnALFs –  
624 computation of the second-order derivatives of the modified  
625 fnALFs;  $NF$  – number of computing functionals (from 1 to  
626 4);  $\eta', \xi', \dots, W'_{rr}$  – cumulative sets of the computations of  
627 functionals;  $\eta, \xi, \dots, W_{rr}$  – final computations of the function-  
628 als. . . . . 48

629 A.11 CPU time for synthesis of disturbing potential using  $M =$   
630 360 versus grid resolution (SFCM - standard forward column  
631 method; MFCM - modified forward column method; ERA -  
632 extended-range arithmetic). . . . . 49

633 A.12 CPU time for synthesis of disturbing potential using  $M =$   
634 2 190 versus grid resolution (SFCM - standard forward column  
635 method; MFCM - modified forward column method; ERA -  
636 extended-range arithmetic). . . . . 50

637 A.13 CPU time for synthesis of disturbing tensor using  $M = 360$   
638 versus grid resolution (SFCM - standard forward column method;  
639 ERA - extended-range arithmetic). . . . . 51  
640 A.14 CPU time for synthesis of disturbing tensor using  $M = 2\ 190$   
641 versus grid resolution (SFCM - standard forward column method;  
642 ERA - extended-range arithmetic). . . . . 52  
643 A.15 CPU time for synthesis of disturbing potential using  $M = 360$   
644 versus number of points (SFCM - standard forward column  
645 method; MFCM - modified forward column method; ERA -  
646 extended-range arithmetic). . . . . 53  
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648  $2\ 190$  versus number of points (SFCM - standard forward  
649 column method; MFCM - modified forward column method;  
650 ERA - extended-range arithmetic). . . . . 54  
651 A.17 CPU time for synthesis of disturbing tensor using  $M = 360$   
652 versus number of points (SFCM - standard forward column  
653 method; MFCM - modified forward column method; ERA -  
654 extended-range arithmetic). . . . . 55  
655 A.18 CPU time for synthesis of disturbing tensor using  $M = 2\ 190$   
656 versus number of points (SFCM - standard forward column  
657 method; MFCM - modified forward column method; ERA -  
658 extended-range arithmetic). . . . . 56

Table A.1: Structure of the input GGM file – spherical harmonic coefficients sorted primarily according to degrees.

$n$	$m$	$\overline{C}_{nm}$	$\overline{S}_{nm}$
2	0	-0.48417E-03	0.00000E+00
2	1	-0.20662E-09	0.13844E-08
2	2	0.24394E-05	-0.14003E-05
3	0	0.95716E-06	0.00000E+00

Table A.2: Structure of the input GGM file – spherical harmonic coefficients sorted primarily according to orders.

$n$	$m$	$\overline{C}_{nm}$	$\overline{S}_{nm}$
2	0	-0.48417E-03	0.00000E+00
3	0	0.95712E-06	0.00000E+00
4	0	0.53998E-06	0.00000E+00
5	0	0.68658E-07	0.00000E+00

Table A.3: Structure of the input file of error variance-covariance matrix – spherical harmonic coefficients sorted primarily according to orders;  $n_{\min} = 2$ ;  $n_{\max} = 3$ ; the column  $CS$  determines whether the variance and covariances in the particular line are related to the coefficient  $\bar{C}_{nm}$  (if  $CS = 0$ ) or to the coefficient  $\bar{S}_{nm}$  (if  $CS = 1$ ).

$CS$	$n$	$m$	variances and covariances of the spherical harmonic coefficients											
0	2	0	4.31E-25											
0	3	0	-2.11E-26	2.48E-25										
0	2	1	3.79E-28	-1.15E-27	3.84E-25									
1	2	1	-3.44E-28	4.67E-28	-1.17E-27	4.16E-25								
0	3	1	1.99E-27	-7.61E-29	2.98E-26	-3.18E-28	2.48E-25							
1	3	1	1.44E-28	-8.80E-29	3.42E-28	2.54E-26	-3.16E-27	2.70E-25						
0	2	2	8.17E-27	-1.72E-27	2.94E-28	3.67E-28	9.06E-29	-1.08E-27	4.02E-25					
1	2	2	1.14E-27	2.94E-28	-5.61E-29	-3.86E-28	-1.23E-27	-1.50E-27	8.37E-28	4.25E-25				
0	3	2	-9.38E-27	6.35E-27	1.08E-27	1.81E-27	7.12E-28	3.53E-28	3.30E-26	9.75E-29	3.07E-25			
1	3	2	-1.27E-28	3.45E-27	1.59E-27	7.97E-28	-1.75E-28	1.15E-28	5.51E-28	2.30E-26	2.78E-27	3.09E-25		
0	3	3	7.74E-28	-1.36E-28	-9.93E-27	5.50E-28	9.55E-28	-3.25E-27	1.06E-27	-8.60E-28	-2.85E-29	1.58E-28	2.74E-25	
1	3	3	-1.14E-27	-2.19E-28	4.51E-28	-1.26E-26	-1.46E-28	4.90E-27	1.25E-28	-1.76E-28	1.18E-28	-5.22E-29	-6.97E-29	2.74E-25

Table A.4: Demonstration of the report file created by the GrafLab.

---

Software	GrafLab 1.00
Generating date	28-Oct-2012
Generating time	13:46:13
Computed	Functionals of the geopotential
Geopotential model file	go_cons_gcf_2_dir_r1.dat
GM of the geopotential model ( $\text{m}^3 \cdot \text{s}^{-2}$ )	3.986004415e+014
R of the geopotential model (m)	6.378136460e+006
Minimum used degree	2
Maximum used degree	240
Reference ellipsoid	GRS80
Latitude limit North (deg)	90.000000000
Latitude limit South (deg)	-90.000000000
Longitude limit West (deg)	0.000000000
Longitude limit East (deg)	360.000000000
Latitude parallels	1801
Longitude parallels	3601
Number of grid points	6485401
Grid height above the ellipsoid (m)	0.000
Computation time (s)	4
Computation of fully normalized ALFs	Standard forward column method

Exported data file contains the following columns:

Latitude (deg)    Longitude (deg)    Disturbing\_potential ( $\text{m}^2 \cdot \text{s}^{-2}$ )

---

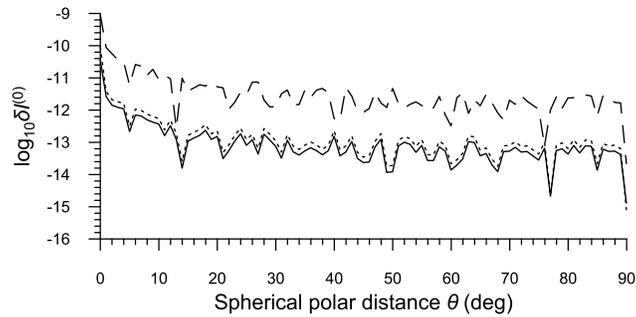


Figure A.1: Base-10 logarithm of the identity error  $\delta I^{(0)}$  of fnALFs using: (i) the standard forward column method (maximum degree:  $M = 1\,800$ ; *solid line*); (ii) the modified forward column method (maximum degree:  $M = 2\,700$ ; *dotted line*); (iii) the extended-range arithmetic (maximum degree:  $M = 65\,536$ ; *dashed line*).

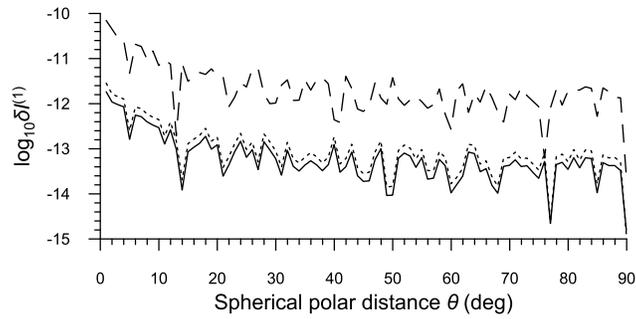


Figure A.2: Base-10 logarithm of the identity error  $\delta I^{(1)}$  of the first-order derivatives of fnALFs using: (i) the standard forward column method (maximum degree:  $M = 1\,800$ ; *solid line*); (ii) the modified forward column method (maximum degree:  $M = 2\,700$ ; *dotted line*); (iii) the extended-range arithmetic (maximum degree:  $M = 65\,536$ ; *dashed line*).

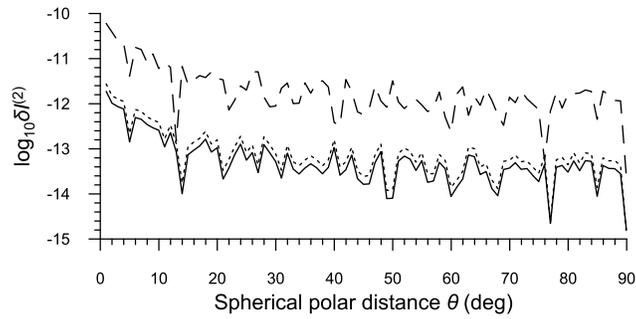


Figure A.3: Base-10 logarithm of the identity error  $\delta I^{(2)}$  of the second-order derivatives of fnALFs using: (i) the standard forward column method (maximum degree:  $M = 1\,800$ ; *solid line*); (ii) the modified forward column method (maximum degree:  $M = 2\,700$ ; *dotted line*); (iii) the extended-range arithmetic (maximum degree:  $M = 65\,536$ ; *dashed line*).

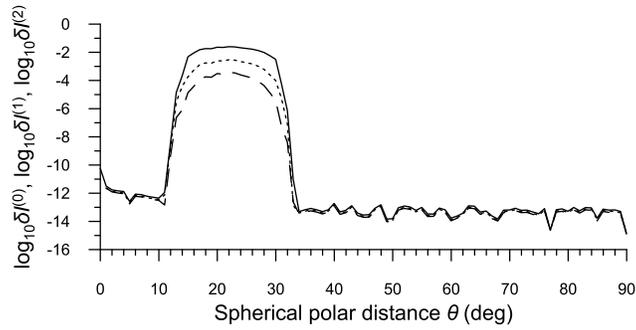


Figure A.4: Base-10 logarithm of the identity errors  $\delta I^{(0)}$ ,  $\delta I^{(1)}$ ,  $\delta I^{(2)}$  of the zero-, first- and second-order derivatives of fnALFs, respectively, using the standard forward column method (maximum degree:  $M = 2190$ ;  $\delta I^{(0)}$  – *solid line*;  $\delta I^{(1)}$  – *dotted line*;  $\delta I^{(2)}$  – *dashed line*).

Geopotential model and reference system selection

Global geopotential model of the Earth

Use maximum degree of GGM

GM of GGM (m3.s-2)      R of GGM (m)

Point type selection

Grid       Load data        Point-wise

phi min (°)      phi step (°)      phi max (°)      phi (°)

lambda min (°)      lambda step (°)      lambda max (°)      lambda (°)

h (m)      h (m)

Calculated parameters and output selection

      Commission error       Export data

            Export report

Figure A.5: GrafLab graphical user interface.

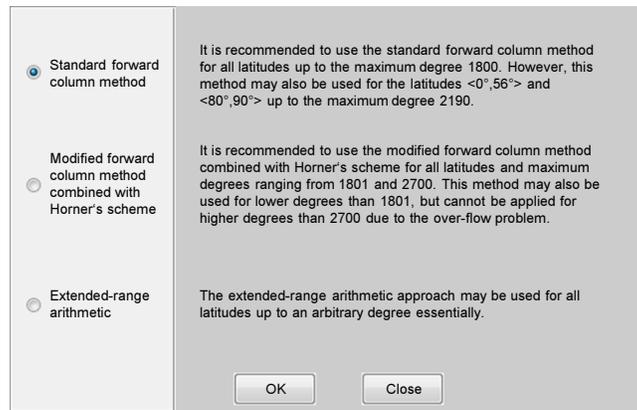


Figure A.6: Computation of fnALFs window.

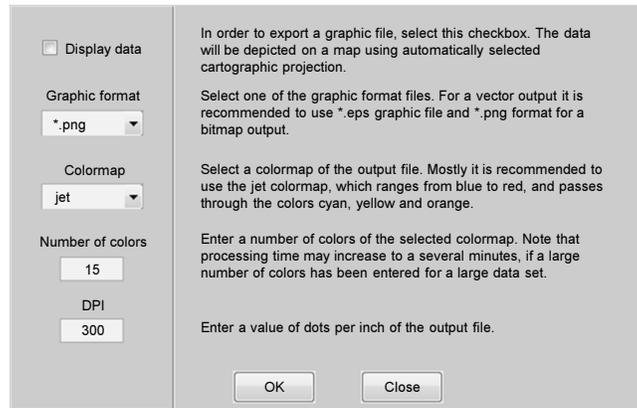


Figure A.7: Display data settings window.

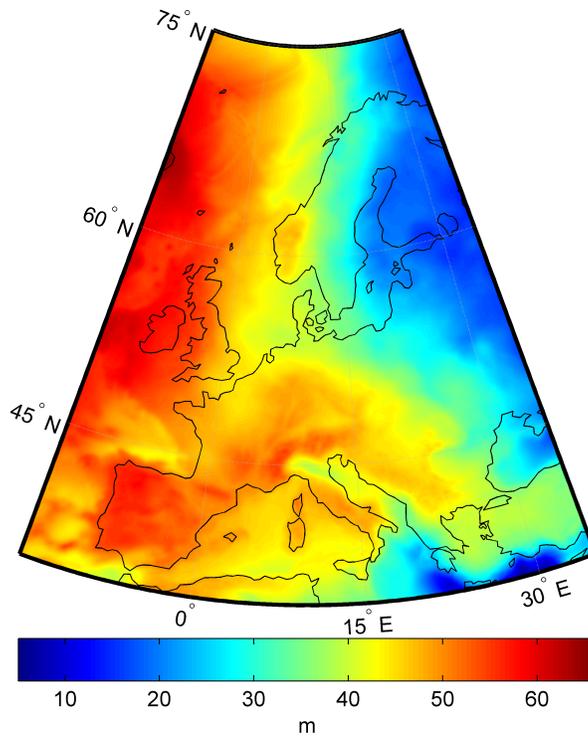


Figure A.8: Geoid undulation computed and depicted using the GrafLab software. The geoid undulation is computed on the regular grid  $\varphi \in \langle 35^\circ, 75^\circ \rangle$ ,  $\lambda \in \langle -15^\circ, 35^\circ \rangle$  with spatial resolution  $0.1^\circ$  using EGM2008 and DTM2006.0 (maximum degree of SHE:  $M = 2\ 190$ ).

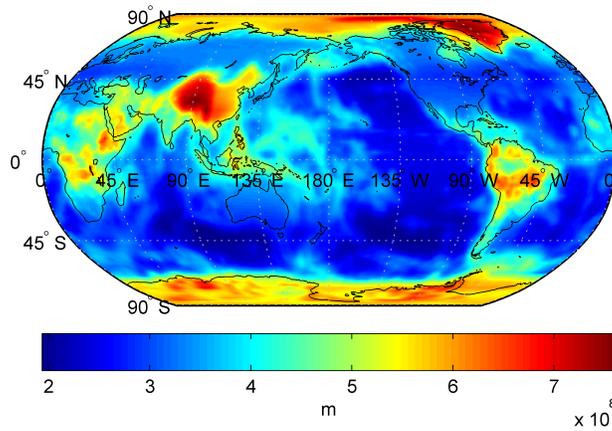


Figure A.9: Commission error of geoid undulation computed and depicted using the GrafLab software. The commission errors of geoid undulation are computed on the regular grid  $\varphi \in \langle -90^\circ, 90^\circ \rangle$ ,  $\lambda \in \langle 0^\circ, 360^\circ \rangle$  with spatial resolution  $2^\circ$  using the full error variance-covariance matrix of GRIM5C1 (maximum degree of SHE:  $M = 70$ ; the error variance-covariance matrix is not calibrated).

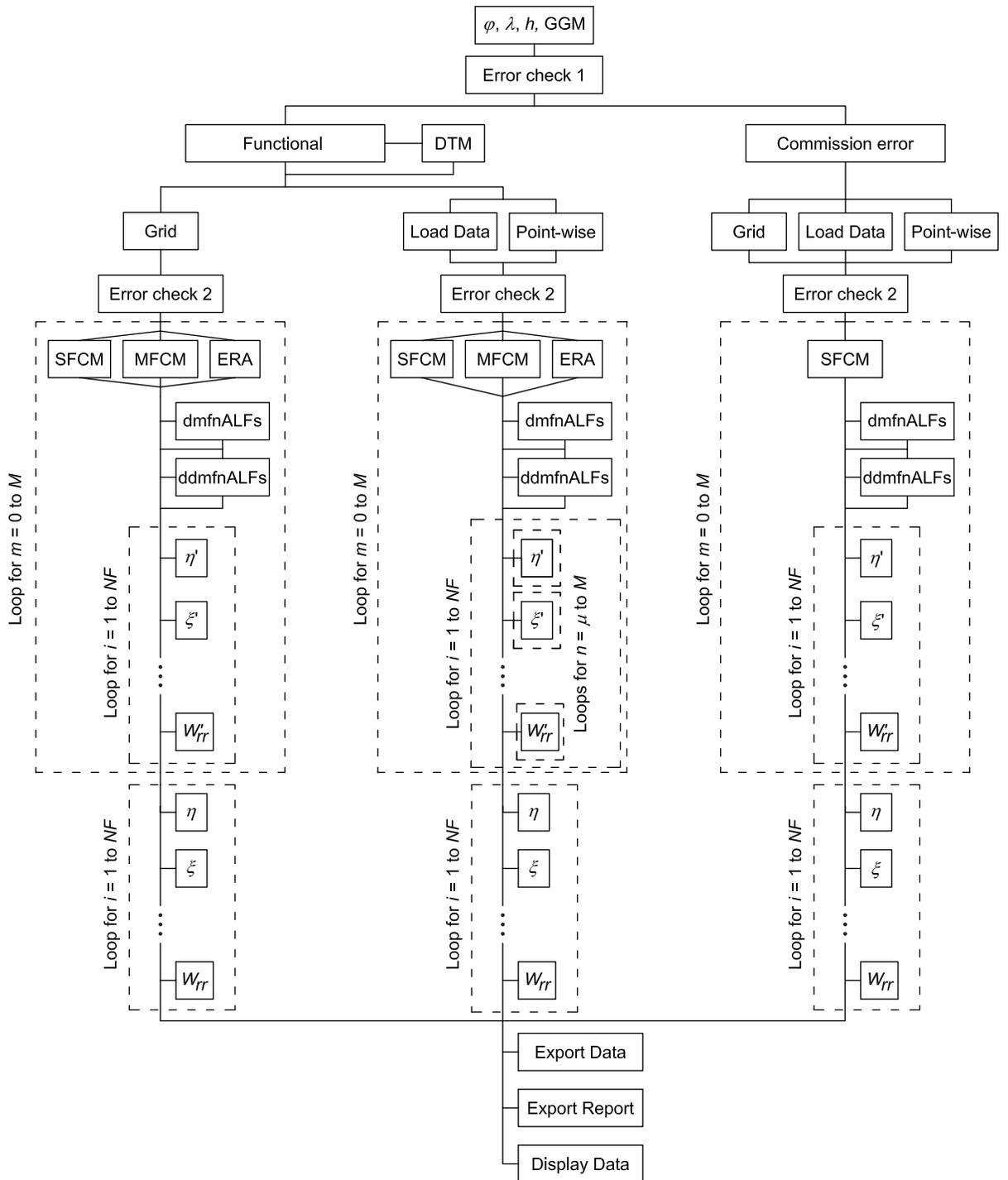


Figure A.10: Flowchart of the GrafLab. Explanation of the symbols and abbreviations in the flowchart:  $\varphi, \lambda, h, \text{GGM}$  – ellipsoidal coordinates of the evaluation points, global geopotential model of the Earth; Error check 1 – the first error check of the input data; DTM – digital terrain model; Error check 2 – the second error check of the input data; Grid, Load data, Point-wise – point type selection; SFCM, MFCM, ERA – computation of the fnALFs using the standard forward column method, the modified forward column method

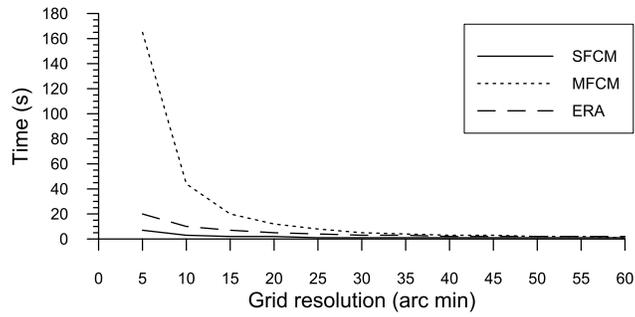


Figure A.11: CPU time for synthesis of disturbing potential using  $M = 360$  versus grid resolution (SFCM - standard forward column method; MFCM - modified forward column method; ERA - extended-range arithmetic).

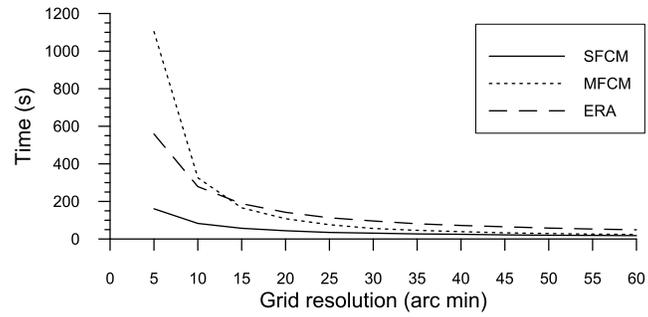


Figure A.12: CPU time for synthesis of disturbing potential using  $M = 2\ 190$  versus grid resolution (SFCM - standard forward column method; MFCM - modified forward column method; ERA - extended-range arithmetic).

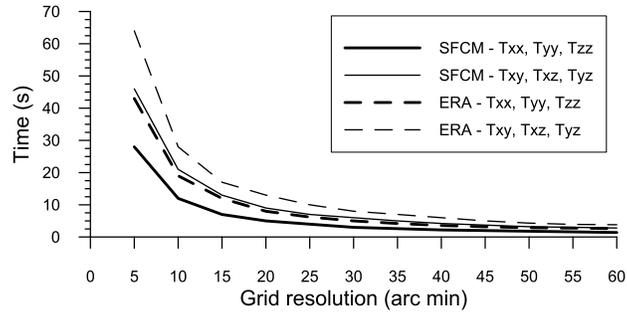


Figure A.13: CPU time for synthesis of disturbing tensor using  $M = 360$  versus grid resolution (SFCM - standard forward column method; ERA - extended-range arithmetic).

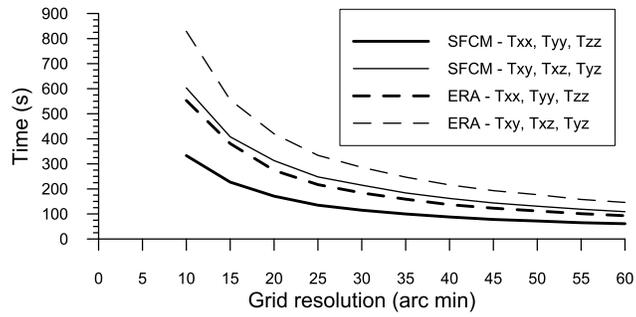


Figure A.14: CPU time for synthesis of disturbing tensor using  $M = 2\ 190$  versus grid resolution (SFCM - standard forward column method; ERA - extended-range arithmetic).

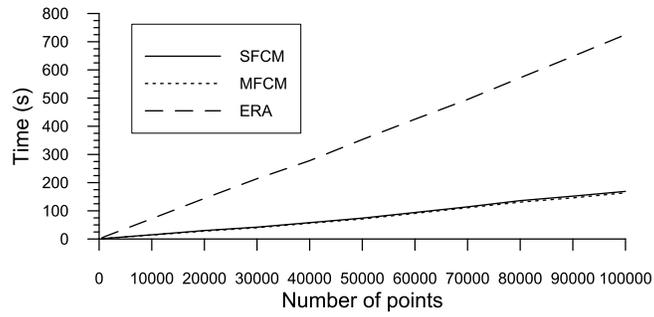


Figure A.15: CPU time for synthesis of disturbing potential using  $M = 360$  versus number of points (SFCM - standard forward column method; MFCM - modified forward column method; ERA - extended-range arithmetic).

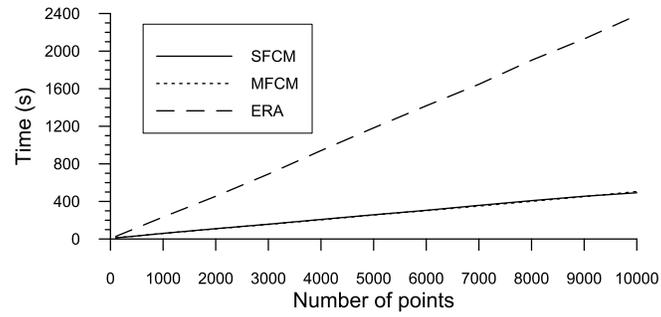


Figure A.16: CPU time for synthesis of disturbing potential using  $M = 2\ 190$  versus number of points (SFCM - standard forward column method; MFCM - modified forward column method; ERA - extended-range arithmetic).

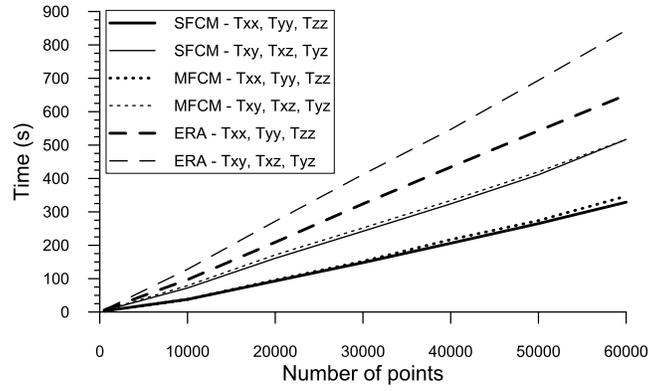


Figure A.17: CPU time for synthesis of disturbing tensor using  $M = 360$  versus number of points (SFCM - standard forward column method; MFCM - modified forward column method; ERA - extended-range arithmetic).

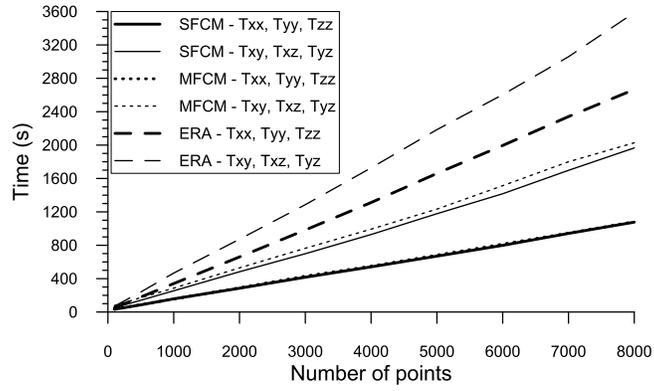


Figure A.18: CPU time for synthesis of disturbing tensor using  $M = 2190$  versus number of points (SFCM - standard forward column method; MFCM - modified forward column method; ERA - extended-range arithmetic).